

Viscoacoustic full waveform inversion: what can be resolved?

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□ Introduction

Gradient calculation by adjoint state

□ Strategies for viscoacoustic FWI



Introduction



Introduction

Viscoacoustic FWI:

Viscoacoustic operator: fit the data and improve the accuracy of velocity

 Multiparameter inversion: velocity and attenuation parameters



Outline

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Adjoint state

Objective function:

$$J[m] = h(p(K,\tau), K, \tau) = \frac{1}{2} \parallel p(K,\tau) - p_{obs} \parallel^2$$

Forward mapping:

$$F(p, v_x, v_z, r_l, K, \tau) = 0$$

$$K = \rho v_p^2$$
$$\tau = \frac{\tau_{\epsilon l}}{\tau_{\sigma l}} - 1$$

relative relaxation time difference

 $au_{\sigma l}$ stress relaxation time

 $au_{\epsilon l}$ strain relaxation time



Adjoint-state method

• Forward modeling equation

$$\begin{cases} \dot{p} = K(v_{x,x} + v_{z,z}) - K \sum_{l=0}^{L} r_l (1 - \tau_{\sigma l} / \tau_{\varepsilon l}) \\ \dot{v_x} = \frac{1}{\rho} \frac{\partial p}{\partial x} \\ \dot{v_z} = \frac{1}{\rho} \frac{\partial p}{\partial z} \\ \dot{r_l} + \frac{1}{\tau_{\sigma l}} r_l = \frac{1}{\tau_{\sigma l}} (v_{x,x} + v_{z,z}) \end{cases}$$

In order to get constant Q model, Generally Maxwell Body(GMB) is included in the forward equaion:

GMB:
$$M(\omega) = M_R + \sum_{l=1}^{L} \frac{iM_l\omega}{\omega_l + i\omega}, \omega_l = \frac{M_l}{\eta_l} = \frac{1}{\tau_{\sigma l}}$$



Adjoint-state method

Adjoint wave equation:

$$\begin{cases} \dot{q} = K(v_{x,x} + v_{z,z}) + K \sum_{l=0}^{L} r_l (1 - \tau_{\sigma l} / \tau_{\varepsilon l}) \\ \dot{v_x} = \frac{1}{\rho} \frac{\partial q}{\partial x} \\ \dot{v_z} = \frac{1}{\rho} \frac{\partial q}{\partial z} \\ \dot{r_l} - \frac{1}{\tau_{\sigma l}} r_l = \frac{1}{\tau_{\sigma l}} (v_{x,x} + v_{z,z}) \end{cases}$$

Gradient for update:

$$grad_{K}J[K,\tau] = -\langle q, DF_{K}[K,\tau] \rangle$$
$$grad_{\tau}J[K,\tau] = -\langle q, DF_{\tau}[K,\tau] \rangle$$

similar cost to acoustic FWI







Q=50



Optimal Checkpointing

Blanch et al (1998); Griewark (1992); Symes(2007):

• For given numbers of time steps and buffers, the recomputation ratio is minimum amongst all possible checkpointing schedules

Question:

• For given numbers of time steps, what is the best choice of the number of buffers?

Solution:

buffers	ratio	d1-ratio
No.	10010	
2	93.282	-65.409
13	4.837	-0.229
19	3.937	-0.140
37	2.934	-0. 016
140	1.999	-0.0131
150	1.985	-1.000e-04
170	1.983	-1.000e-04
190	1.981	-1.000e-04

Table 1: List of priority number of buffers (≤ 200)





Gradient calculated by adjoint state

Compensation

$$d(x,t) = d(x,t)e^{2\pi\omega_0 t/2Q_a}$$

- ω_0 corresponding to peak frequency
- Q_a Average quality factor



Gradient



Acoustic

Viscoacoustic



Gradient



Viscoacoustic

Viscoacoustic compensation



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Ture models and observed data



Research in T.R.I.P.



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Ture models and observed data

- Shot: 10;
- Receriver:1001, surface;
- Source :20HZ
- Offset_max: 10000m
- Data:full wave, viscoacoustic

stopping criterion for iteration

 $|gradient|_{max} <= 0.1 |gradient_{initial}|_{max}$





Data: all the information









Initial V:smooth

Initial Q :smooth

Data: all the information









Initial V:smooth









Conclusion

- For reflection data, v_p and Q are strongly coupled . Incorrect Q results in incorrect reflector amplitudes. Long wavelength Q structure is not updated. The large aperture reflection contains limited long wavelength Q.
- For refraction data , information about long wavelength Q structure presents in the data, and this permits update of Q.
- The update of Q contains more short scale structure than that of velocity, and is easier to fall into local solution, especially for the case that the velocity is far from the true one.



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Thank you



Research in T.R.I.P.