Implementation of PML in the Depth-oriented Extended Forward Modeling

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The Rice Inversion Project (TRIP)

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Objective

Numerically solving the wave propagation problem in a bounded region.

Solution

Absorbing Boundary Conditions (ABCs) Perfectly Marched Layers (PML)

- 1994, Berenger, split-field PML for use with Maxwell's equations.
- 1996, Gedney, **uniaxial PML** or **UPML**, described as an artificial anisotropic absorbing material.
- 2010, Marcus J. Grote, "Efficient PML for the wave equation". (fewer auxiliary variables)

Denote \hat{u} as the Laplace transform of u

$$\hat{u}(\mathbf{x},s) = \int_0^\infty e^{st} u(\mathbf{x},t) dt \tag{1}$$

Outside of the computational domain Ω , \hat{u} then satisfies the Helmholtz equation,

$$s^{2}\hat{u} = \frac{\partial}{\partial x_{1}} \left(c^{2} \frac{\partial \hat{u}}{\partial x_{1}} \right) + \frac{\partial}{\partial x_{2}} \left(c^{2} \frac{\partial \hat{u}}{\partial x_{2}} \right) + \frac{\partial}{\partial x_{3}} \left(c^{2} \frac{\partial \hat{u}}{\partial x_{3}} \right)$$
(2)

• Next, we introduce the coordinate transformation

$$x_i \mapsto \tilde{x_i} := x_i + \frac{1}{s} \int_0^{x_i} \zeta_i(x) dx, i = 1, 2, 3$$
 (3)

where ζ_i is the damping profile.

• Partial differentiation:

$$\frac{\partial}{\partial \tilde{x}_i} = \frac{s}{s + \zeta_i} \frac{\partial}{\partial x_i} \tag{4}$$

• If \hat{u} satisfies the modelfied Helmholtz equation, then

$$s^{2}\hat{u} = \frac{\partial}{\partial \tilde{x}_{1}} \left(c^{2} \frac{\partial \hat{u}}{\partial \tilde{x}_{1}} \right) + \frac{\partial}{\partial \tilde{x}_{2}} \left(c^{2} \frac{\partial \tilde{u}}{\partial \tilde{x}_{2}} \right) + \frac{\partial}{\partial \tilde{x}_{3}} \left(c^{2} \frac{\partial \hat{u}}{\partial \tilde{x}_{3}} \right)$$
(5)

• Then, by replacing partial derivatives $\frac{\partial}{\partial \tilde{x}_i}$ by $\frac{\partial}{\partial x_i}$, and transforming back to time domain, we get the PML modified wave equation:

$$u_{tt} + (\zeta_1 + \zeta_2 + \zeta_3)u_t + (\zeta_1\zeta_2 + \zeta_2\zeta_3 + \zeta_3\zeta_1)u = \nabla \cdot (c^2 \nabla u) + \nabla \cdot \Phi - \zeta_1\zeta_2\zeta_3\psi$$

$$\Phi_t = \Gamma_1 \Phi + c^2 \Gamma_2 \nabla u + c^2 \Gamma_3 \nabla \psi$$

$$\psi_t = u$$
(6)

$$\begin{split} \Gamma_1 = \begin{bmatrix} -\zeta_1 & 0 & 0\\ 0 & -\zeta_2 & 0\\ 0 & 0 & -\zeta_3 \end{bmatrix}, \Gamma_2 = \begin{bmatrix} \zeta_2 + \zeta_3 - \zeta_1 & 0 & 0\\ 0 & \zeta_3 + \zeta_1 - \zeta_2 & 0\\ 0 & 0 & \zeta_1 + \zeta_2 - \zeta_3 \end{bmatrix},\\ \Gamma_3 = \begin{bmatrix} \zeta_2 \zeta_3 & 0 & 0\\ 0 & \zeta_3 \zeta_1 & 0\\ 0 & 0 & \zeta_1 \zeta_2 \end{bmatrix} \end{split}$$

The choice of damping profiles $\zeta_i(x_i)$:

$$\zeta_i(x_i) = \bar{\zeta}_i \left[\frac{|x_i - a_i|}{L_i} - \frac{\sin\left(\frac{2\pi|x_i - a_i|}{L_i}\right)}{2\pi} \right], a_i \le |x_i| \le a_i + L_i$$
(7)

The relative reflection, R, is given by

$$\bar{\zeta}_i = \frac{c}{L_i} \log\left(\frac{1}{R}\right) \tag{8}$$

- Constant velocity c = 3
- Grid spacing: $\Delta x = \Delta z = 0.01$
- Domain size: 5×5
- Thickness of PMLs: L = 0.5
- Source: Ricker wavelet at the center. $(f_{peak} = 10Hz)$

t=0.2 s



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t = 0.5 s



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t = 0.9 s



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t = 1.0 s



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t=1.1 s



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t=1.2 s



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t=1.3 s



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t=1.4 s



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t=1.5 s



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t=1.6 s



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t=1.7 s



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t=1.8 s



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t=1.9 s



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 $t{=}10.0 s$

t=0.2 s



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t = 0.5 s



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t = 0.9 s



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t = 1.0 s



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t=1.1 s



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t=1.2 s



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t = 1.3 s



t=1.4 s



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t=1.5 s



t = 1.6 s



t=1.7 s



t=1.8 s



t=1.9 s



t=10.0 s



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PML in Extended modeling

- Implement PML in depth-oriented extended forward modeling.
- The PML does suppress the reflections exfficiently.
- Simplicity and the fewer auxiliary variables.
- Furture work
 - R vs. $\overline{\zeta}$, Δx_i , θ , ...
 - Choice of $\zeta(x)$ function
 - ABCs vs. PML
 - $2D \rightarrow 3D$

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